

# Synchrophasor Implementations

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# Topics of Discussion

- Description of Manitoba WAMS
- Introduction to Birchtree SVC Project
- Commissioning Results
- Lessons Learned and Future Road Map

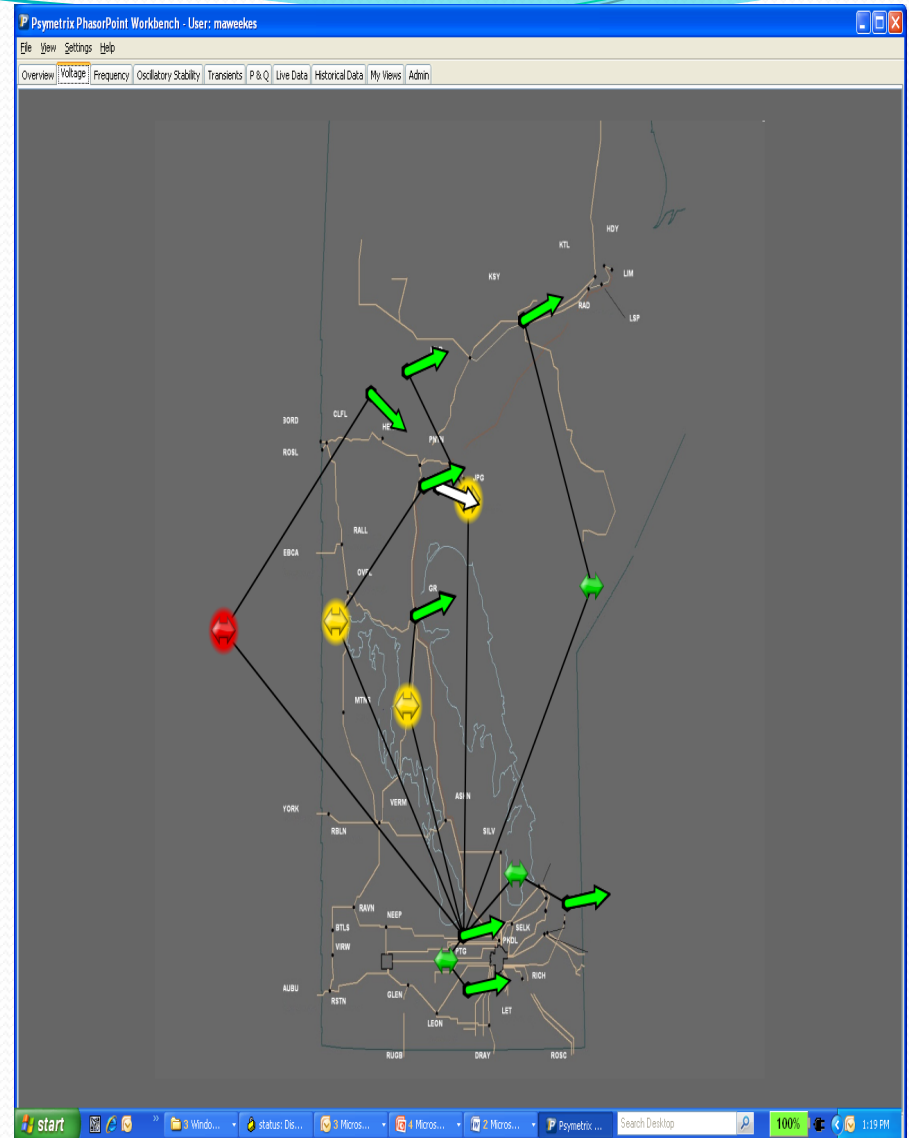
Organization	PDC		PMU	
	Contracted	Connected	Confirmed Sites	Connected Devices
Ameren	1	1	21	6
American Trans Co.	N/A	1	N/A	5
Duke Energy	1	1	16	4
Great Rivers Energy	1	1	8	2
Hoosier Energy	1	1	7	9
Indianapolis P&L	1	1	6	7
International Trans Co.	1	1	12	5
<b>Manitoba Hydro</b>	<b>2</b>	<b>1</b>	<b>22</b>	<b>6</b>
MidAmerican Energy	1	0	12	0
Minnesota Power	1	1	4	1
Montana Dakota Utilities	0	0	5	0
Northern Indiana Public Service	3	1	8	2
Ottertail Power	2	1	6	3
Vectren	1	0	3	0
WAPA	0	0	4	0
XCEL Energy	0	0	11	0
<b>TOTAL</b>	<b>16</b>	<b>11</b>	<b>145</b>	<b>50</b>

# Need for wide Area Measurements

- Typical PSS tuning monitors local signals
- Problems can arise with fighting between controllers
- Advantage of monitoring a wide area can be addressed with synchrophasors

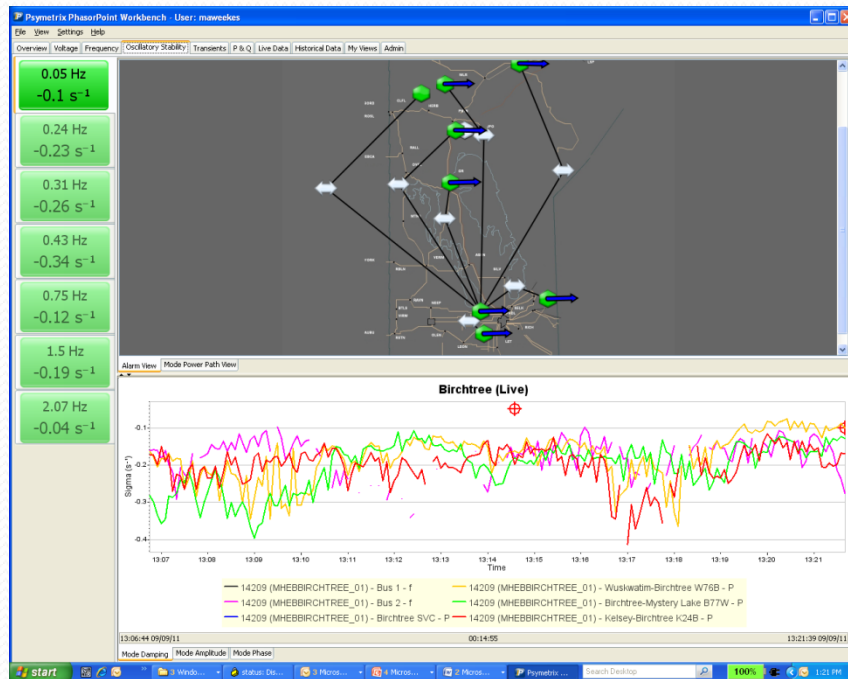
# WAMS

- Phasorpoint tool used primarily to see the modes on the system

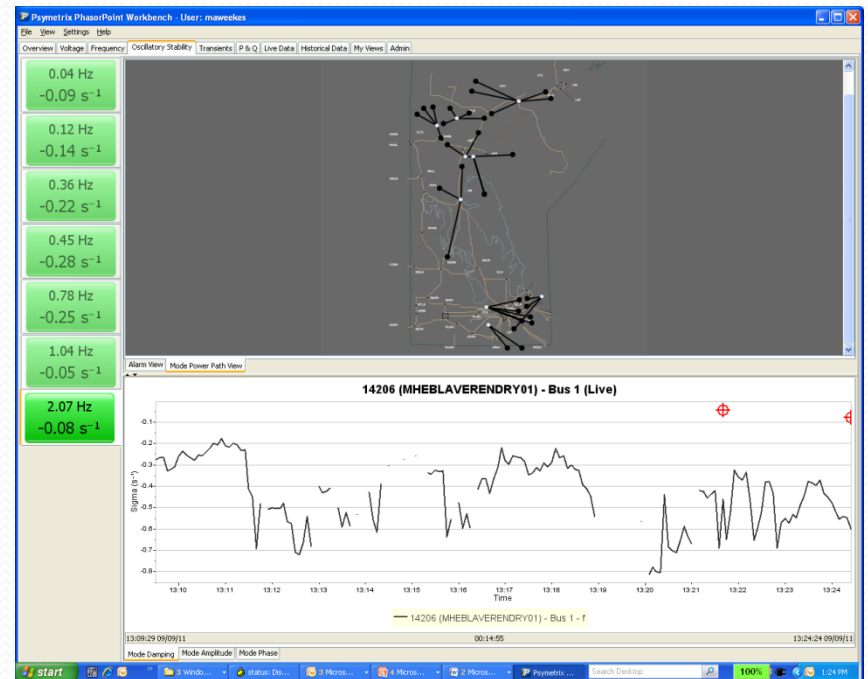


# Phasor Point

## Mode Charting



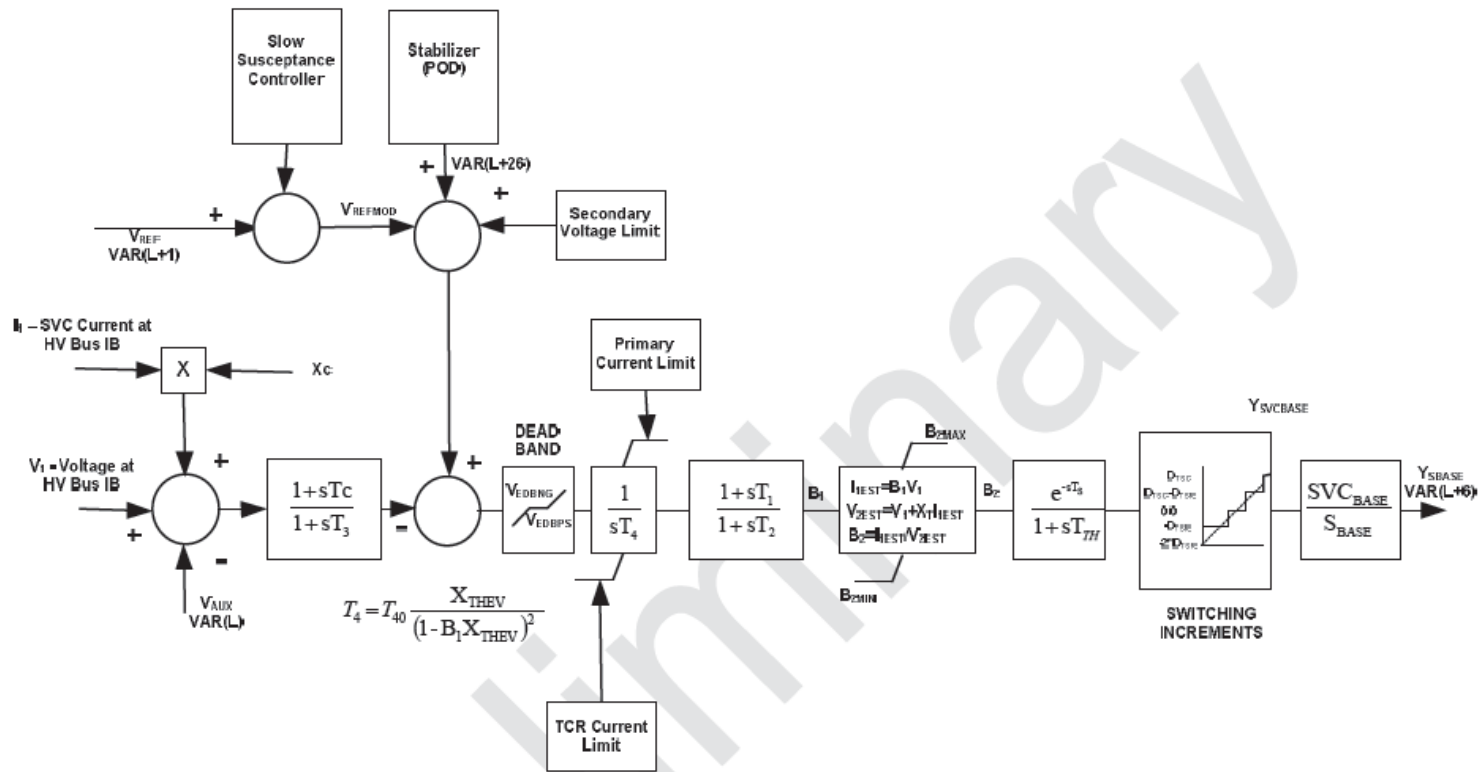
## Mode Power Path



# Sites Chosen

- known inter-area modes in our Northern ac.
- sensitivities of modes to various power flow conditions
- Upcoming projects in Northern ac
- Future sites will increase from 6 to 30 PMU locations
- Using existing TFR devices

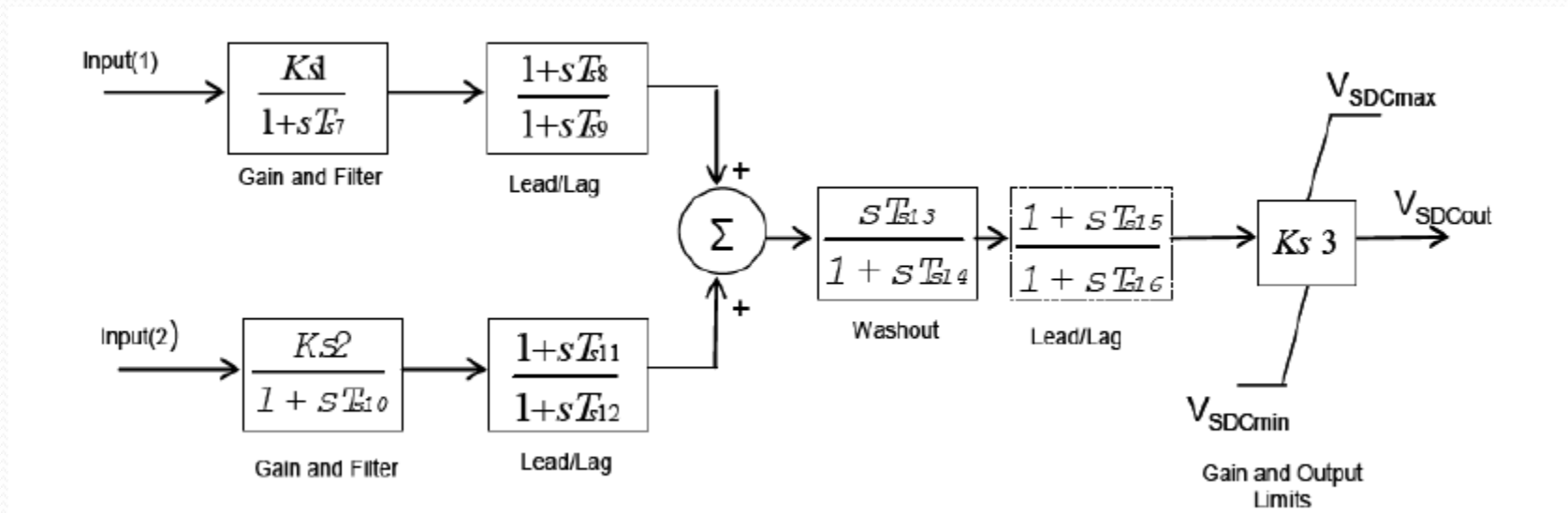
# Birchtree SVC Controller



BTSVC – Voltage Controller



# Power Oscillation Damper (POD)



# Commissioning Objectives

- Transfer function verification of the SVC voltage and POD controllers
- Tuning the POD to provide good damping performance for the modes within the frequency range of interest 0.5 to 0.9 Hz
- Minimize the interaction between the Ponton SVC and Birchtree SVC
- Optimize the Birchtree SVC POD and Ponton SVC SDC settings for most northern ac system generation patterns and operating conditions

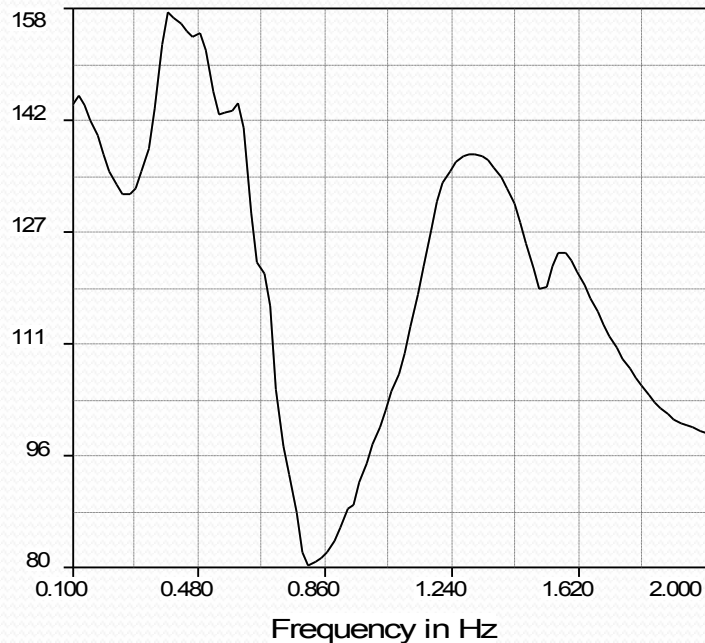
# Risks and Mitigations

- Output is correctly controlled from input, as expected
- Check the degree of movement in the rest of the system in response to a step change
- Confirm consistency with time-domain measurements
- Decide criteria for “unacceptable” oscillations.
- Switch controllers off one-by-one or plant-by-plant, separated by a period of time.

# System Frequency Response

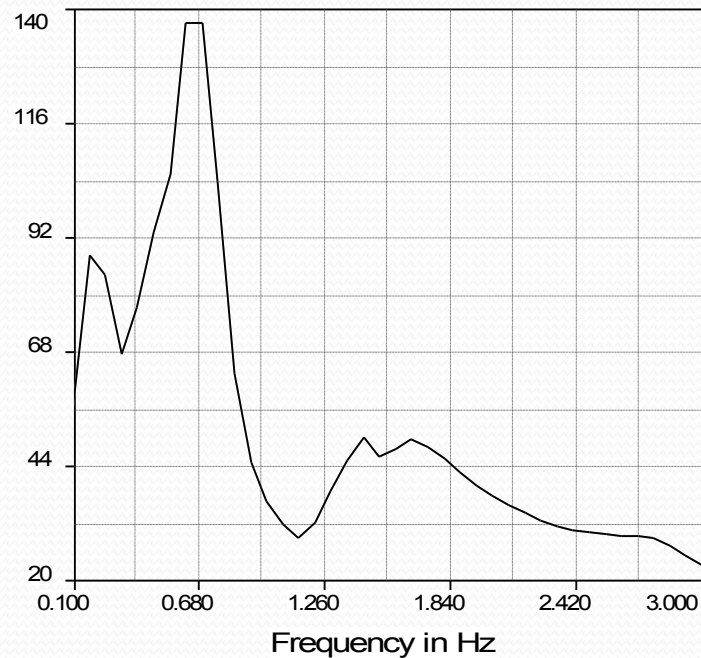
- Model verification (frequency response) of SVC POD design

Bus voltage angle(deg)



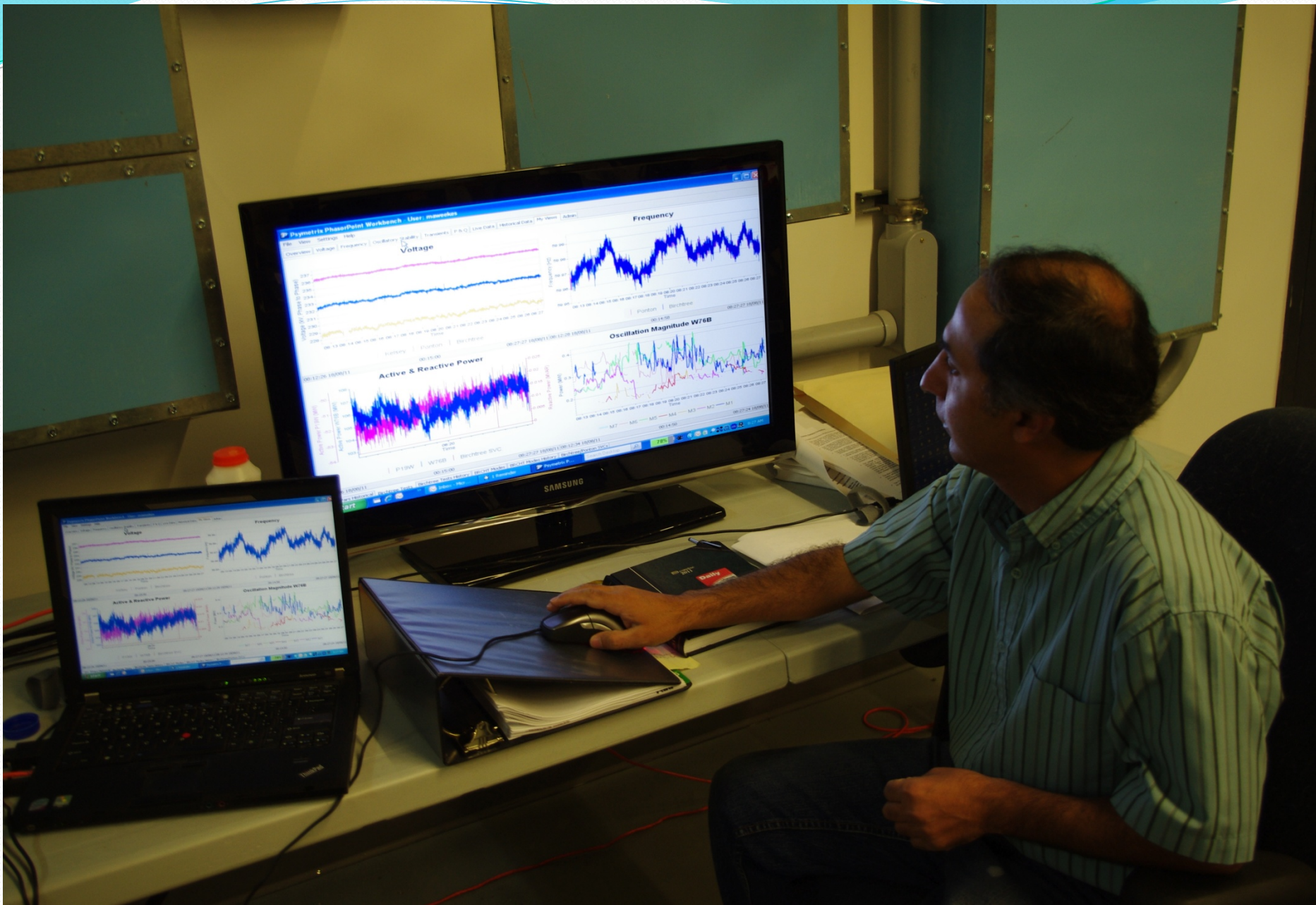
Phase

Bus voltage angle(deg)



Magnitude

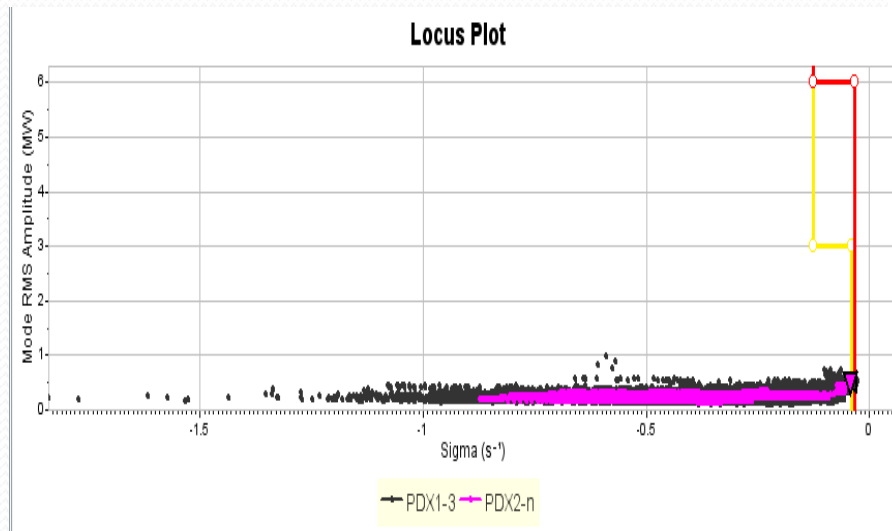
The frequency response characteristic (magnitude and phase) of the transfer function between Birchtree SVC input and voltage angle (frequency



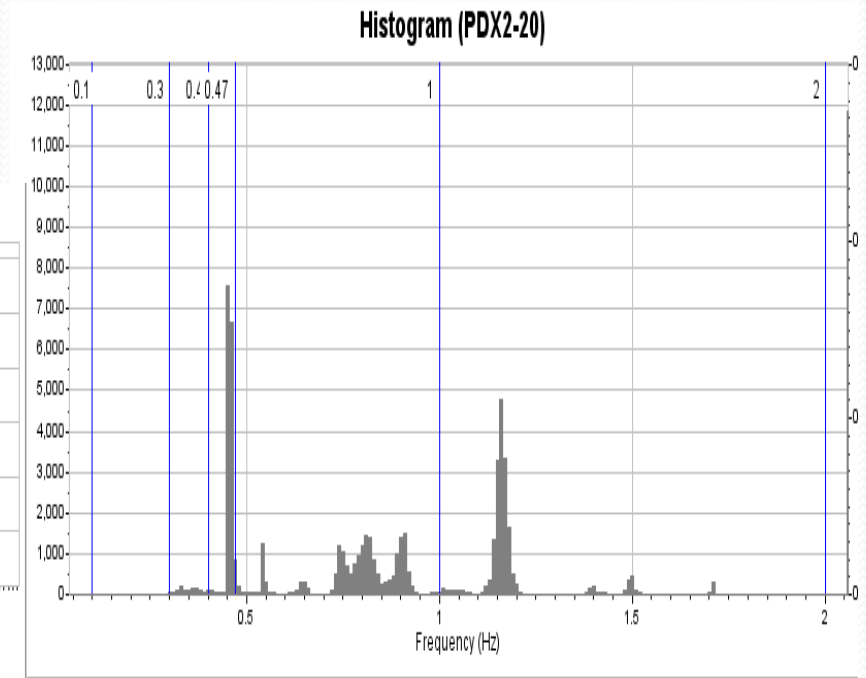
# Mode Trending

## Root locus of mode

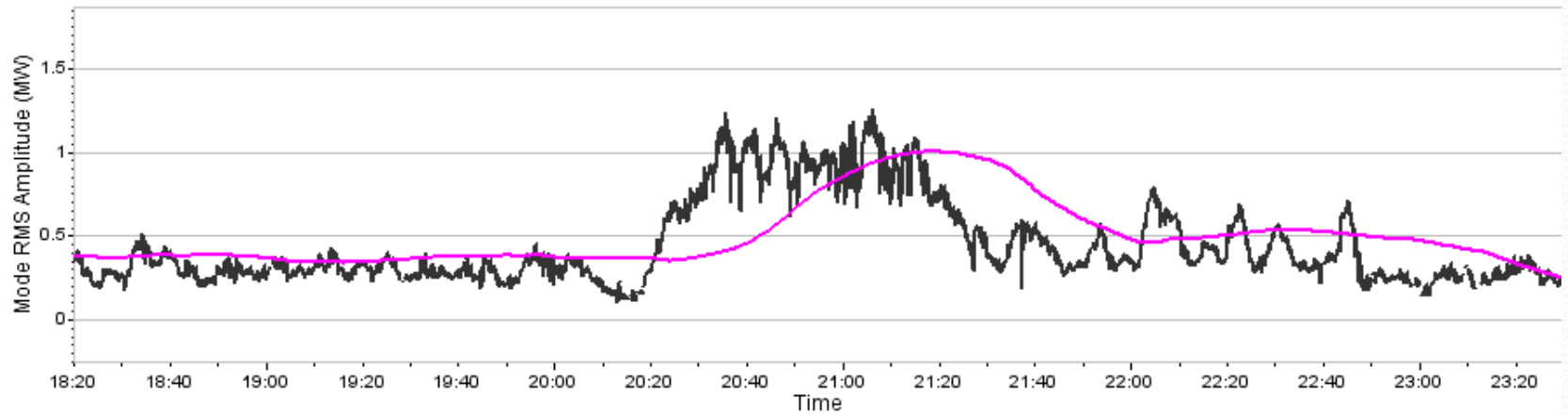
- Trending and verification of damping controller performance



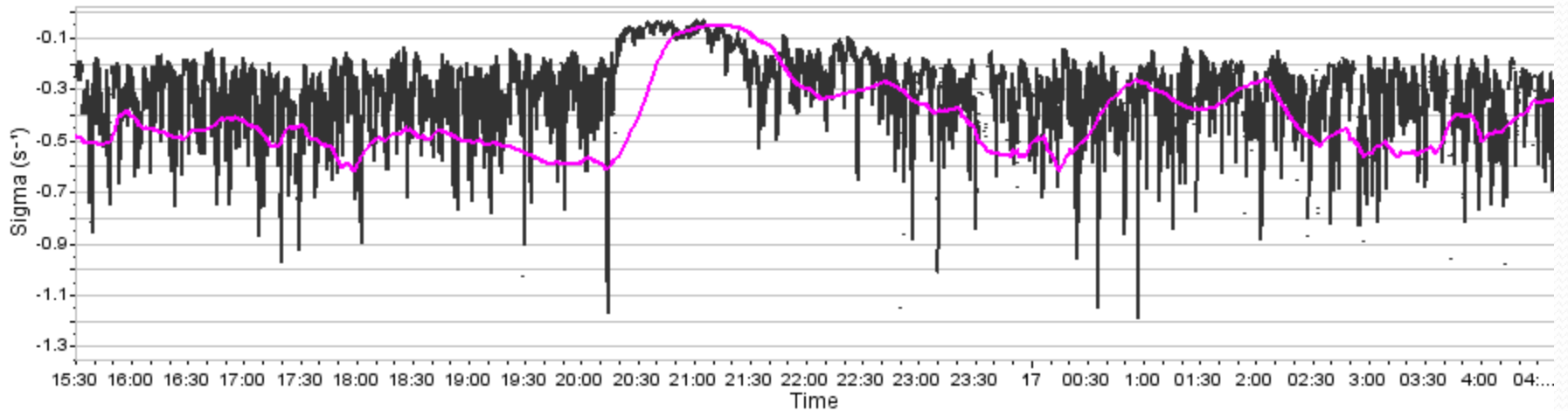
## Observability of the mode over time



### Mode Amplitude



### Mode Damping



— PDX1-3 — PDX2-n

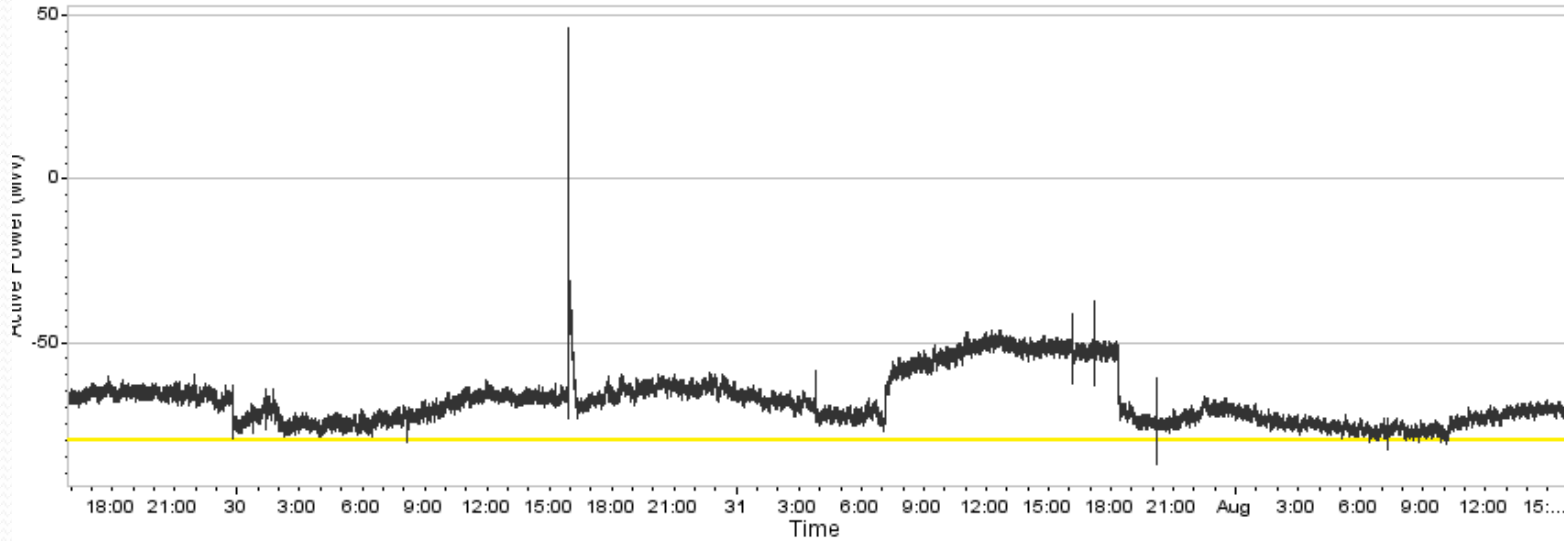
# Unexpected Results Captured

- Mode increases with lower power
- Initial response of POD with other settings
- Clock error

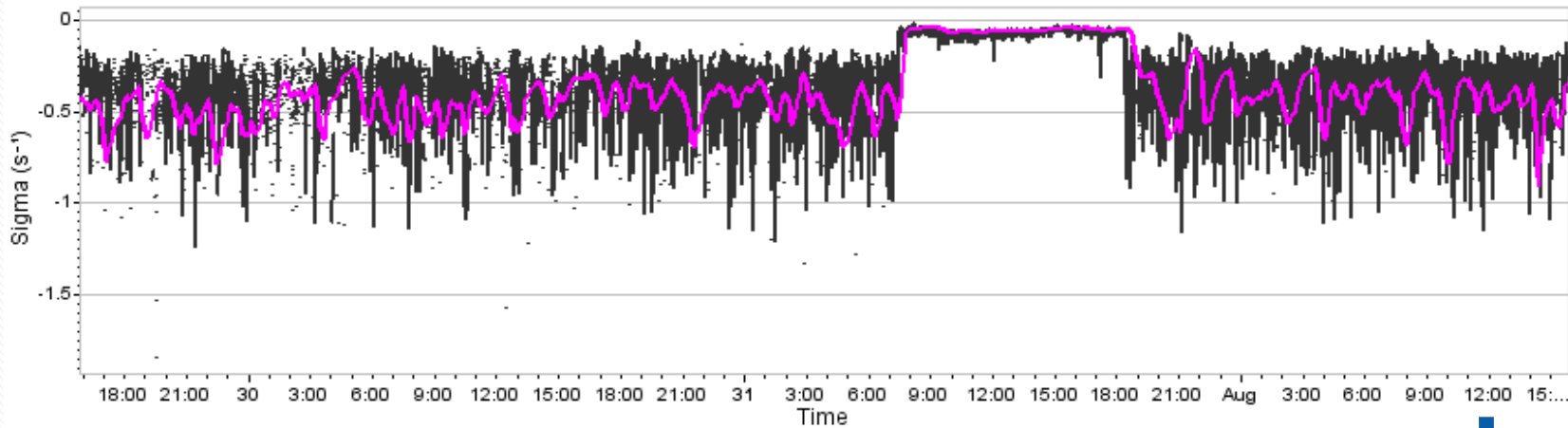


# Cont....System Baseline

### Active Power



### Mode Damping

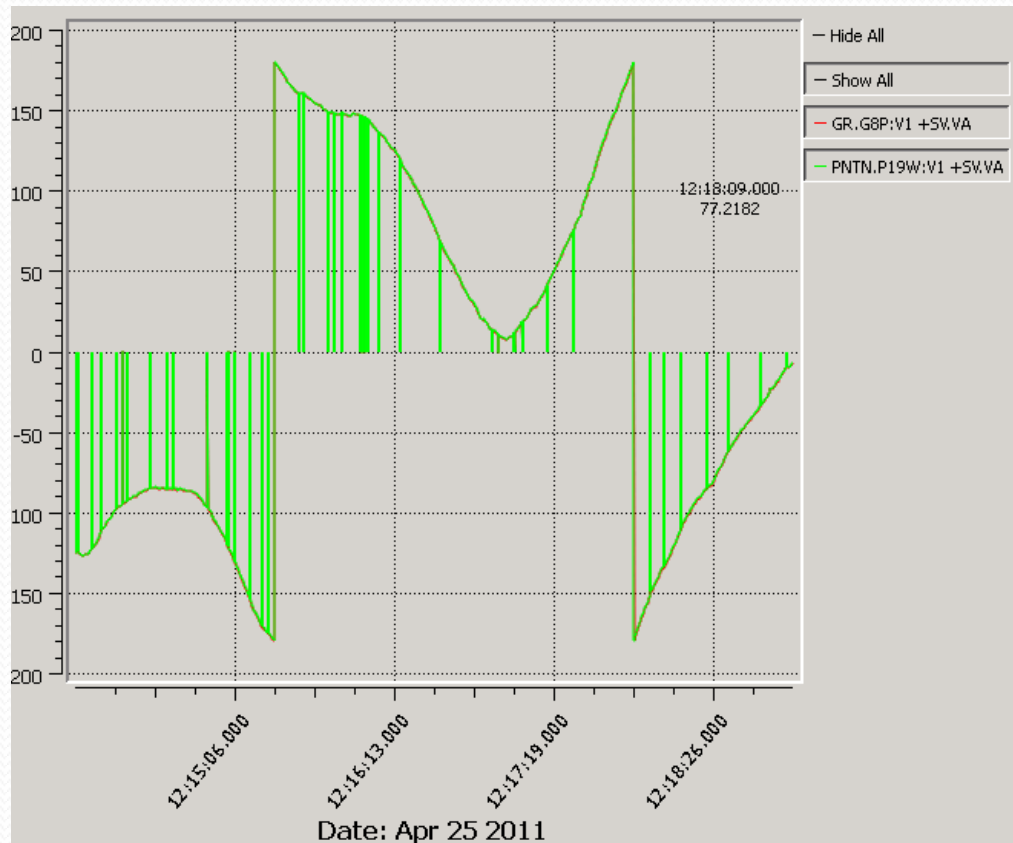


— PDX1-3 — PDX2-n

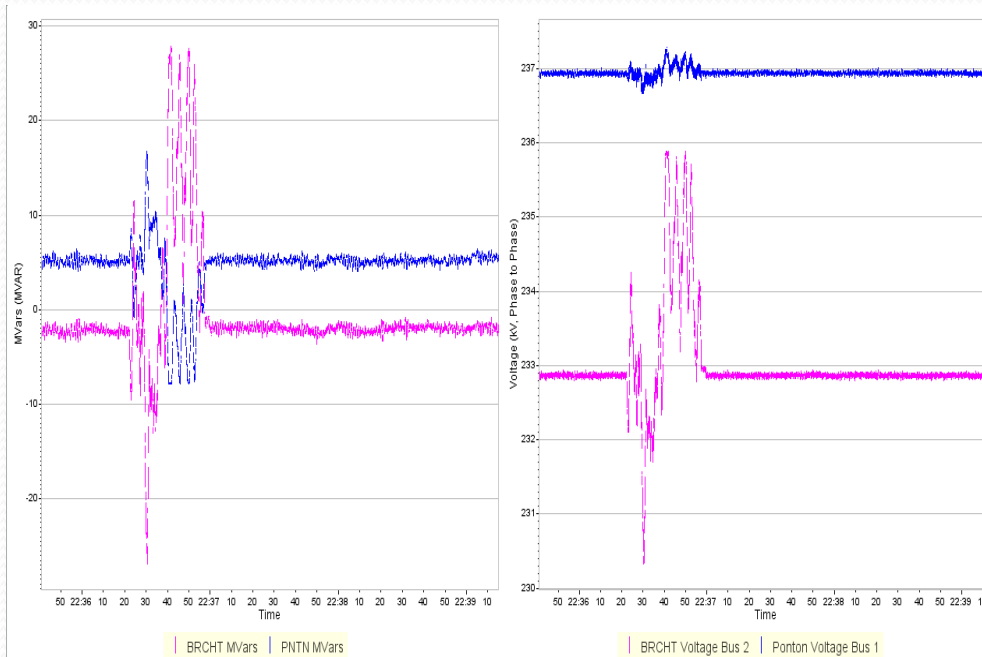
# Cont....System Baseline

April 25, 2011 – 11:14:00 to 11:19:00 – Approx. 2 hours before event

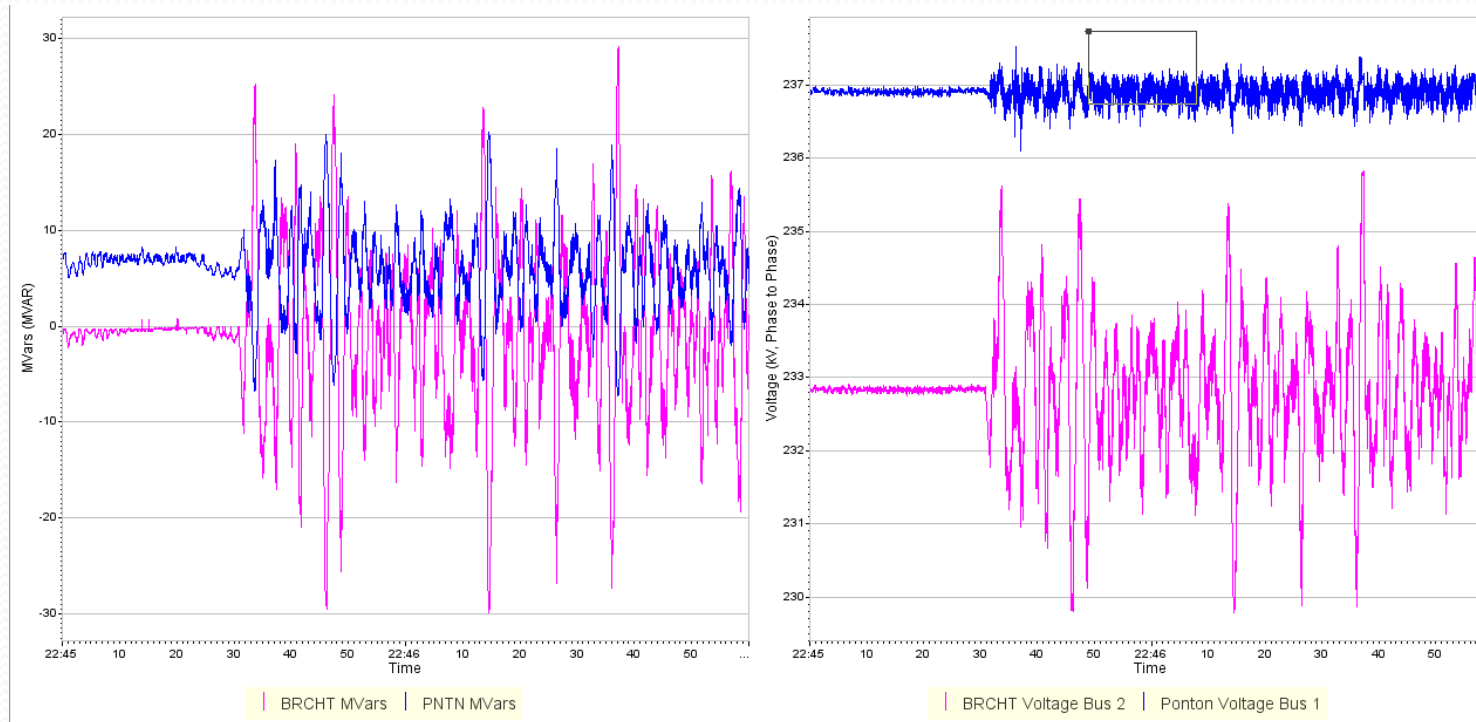
## Clock Errors



# POD First Settings

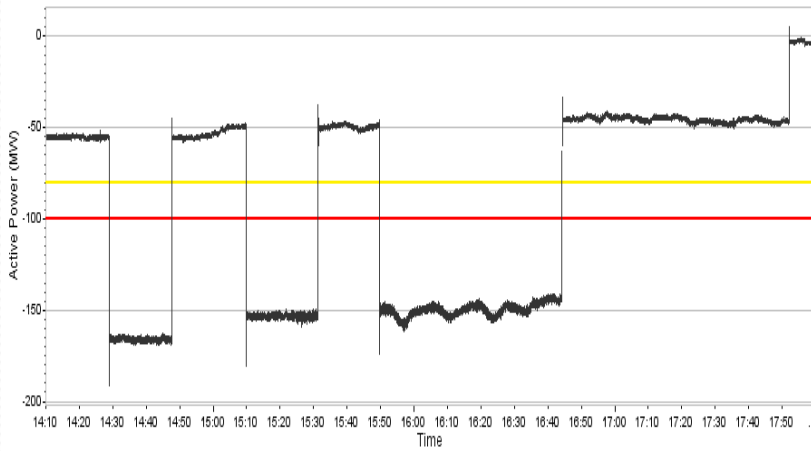


# POD Second Settings

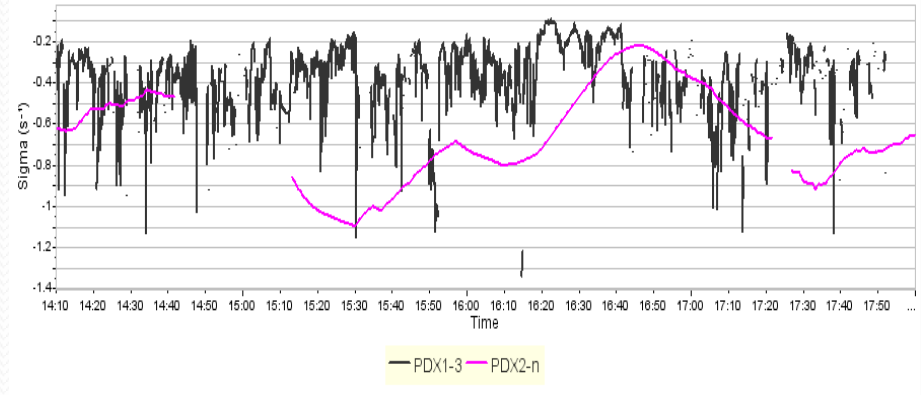


# Open/Close line test

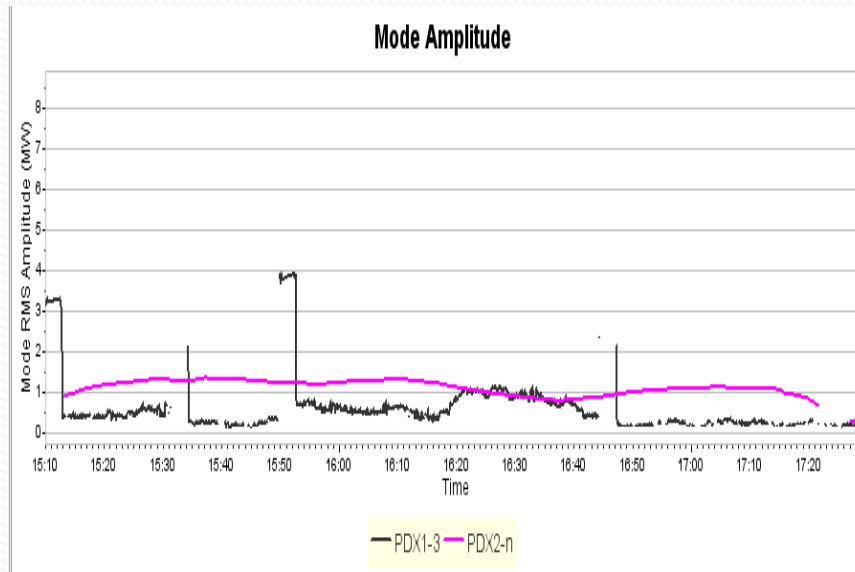
Active Power



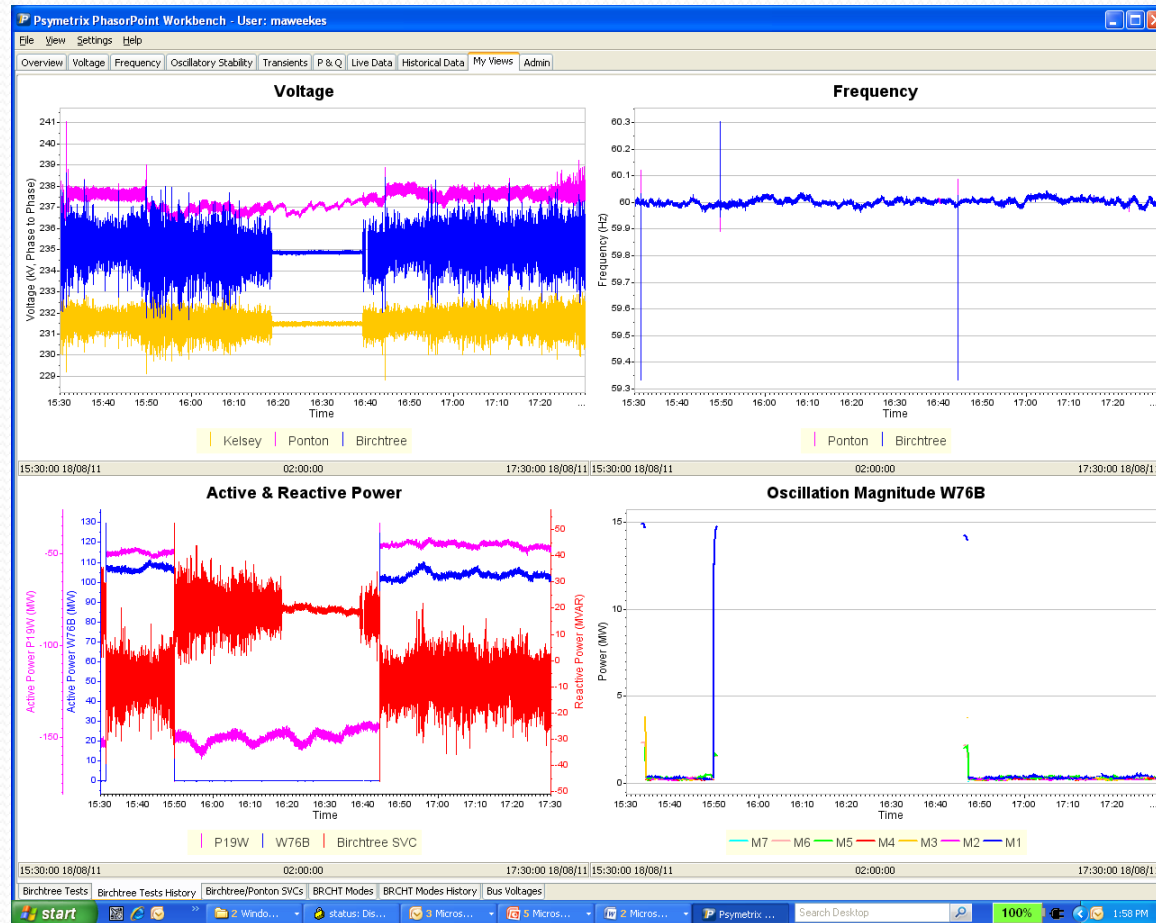
Mode Damping



Mode Amplitude



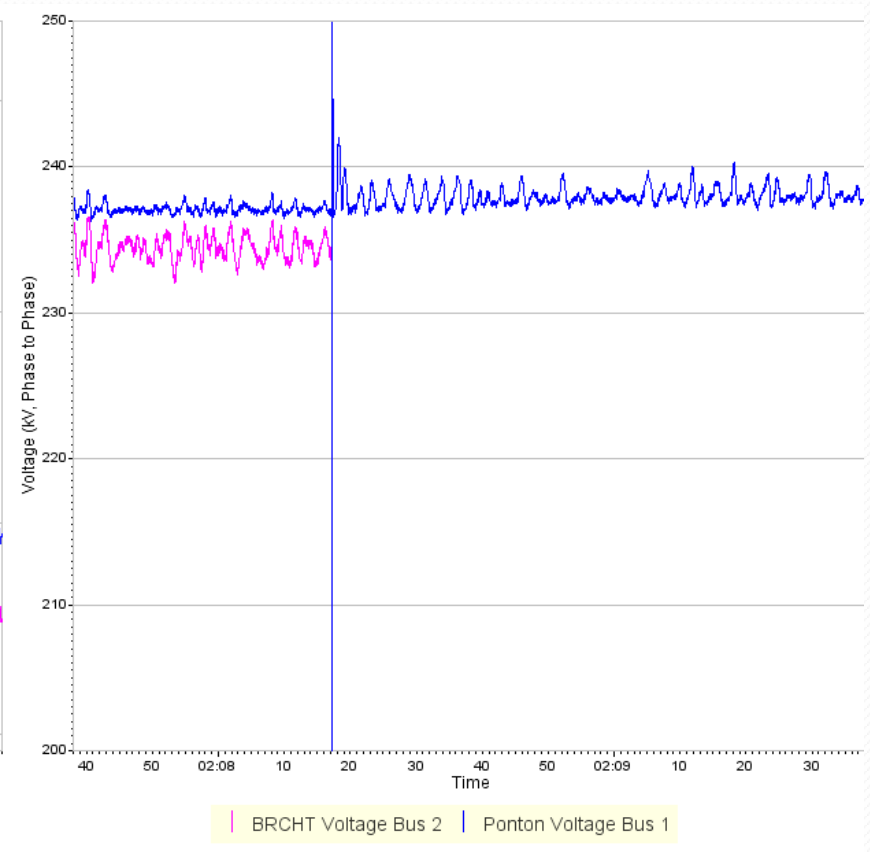
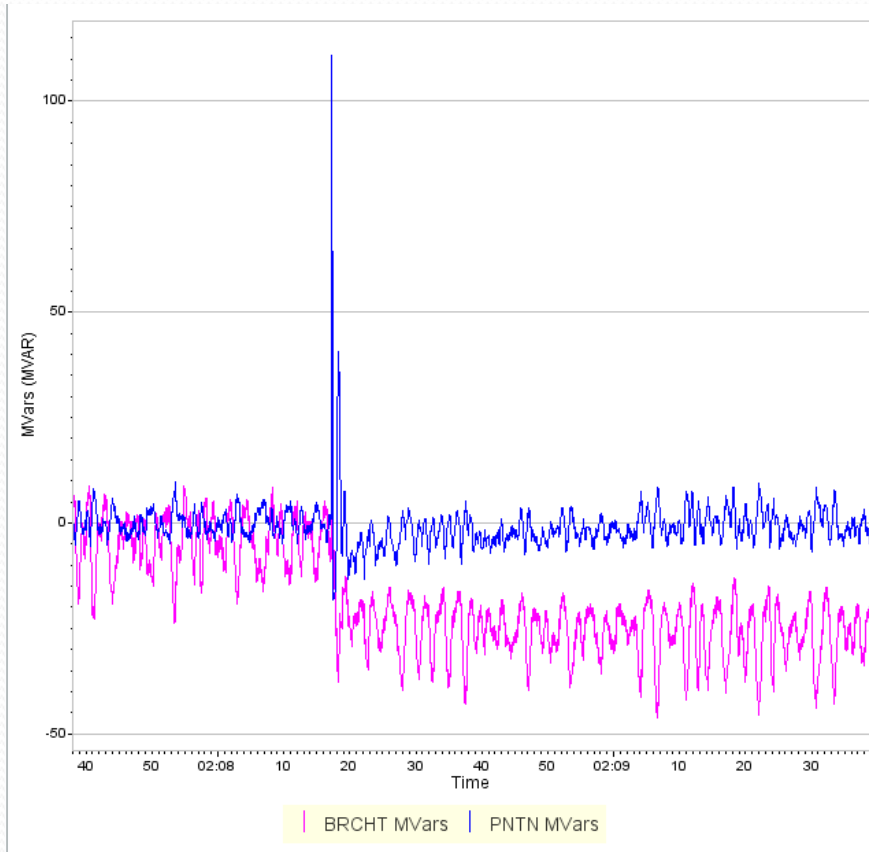
# Open/Close Line Test



# Open/Close Line Test



# SLG Fault





# Lessons Learned

- **Channel Selection** (problem with power calculation if switching occurs)
- Importance of doing a **frequency response** initially to confirm models
- **Real time feedback** to see if and how multiple power system controllers may fight with each other.
- **Clock errors can be significant** and need mitigation measures both in real time and regular maintenance
- **Integration of analog signals** in the future to PMU data (also significance of proper channel selection and sites)
- **Unusual Modes were identified** as consistently observed on the system but low in magnitude

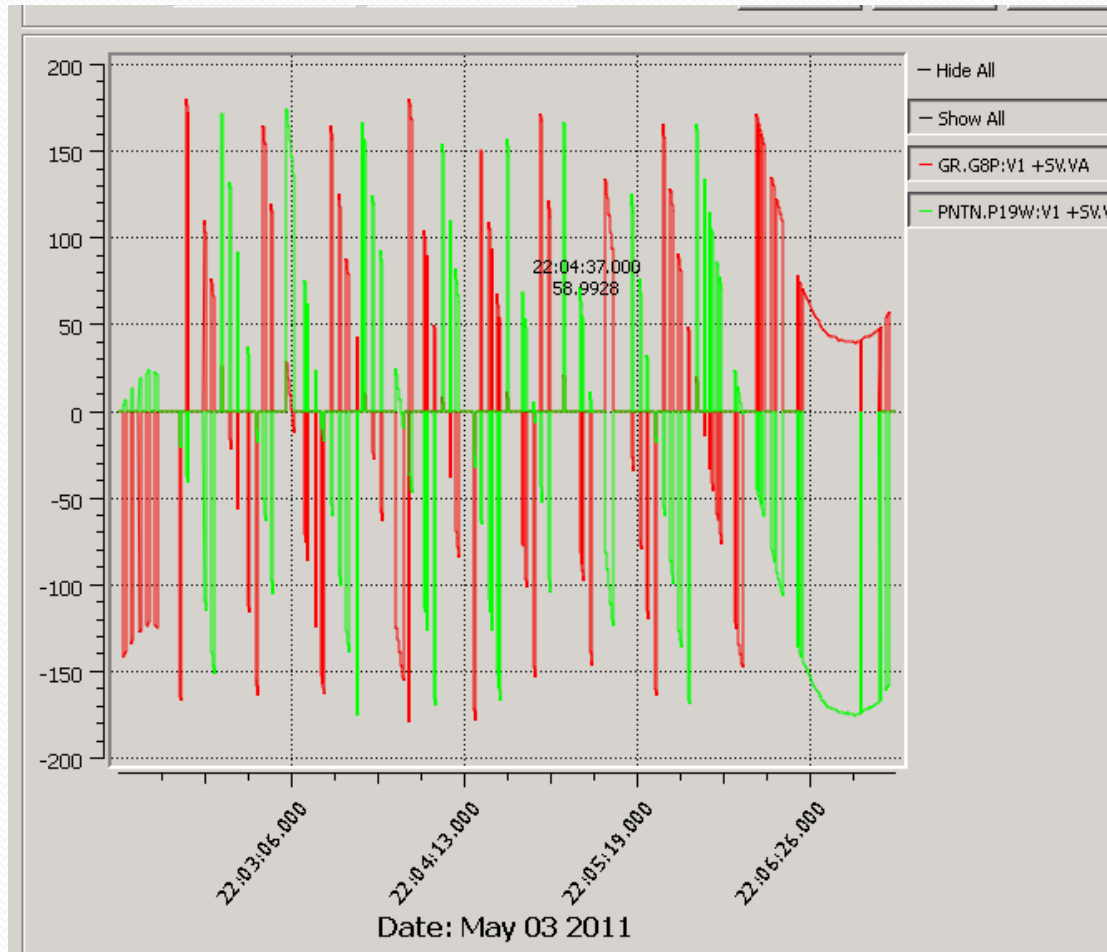
# Future Road Map

- Model verification (complement NERC testing)
- Investigations to increase transfer limits through compound event analysis
- Investigation of islanding and coherency of generators
- Integration with real time tools that use power models (benchmarking)
- EMS state estimator improvement especially after the full complement of PMUs are on the system

Questions ??

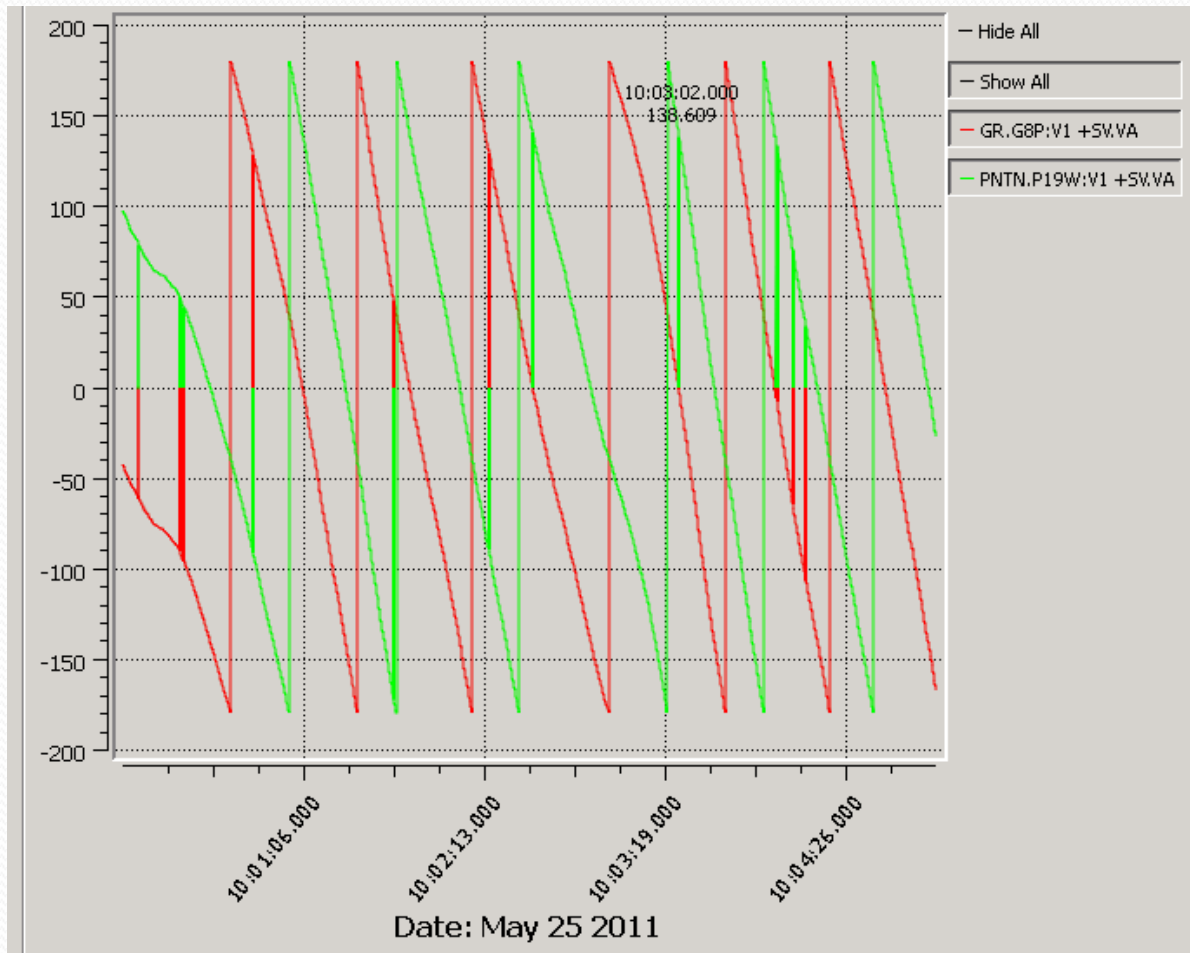
# Cont....System Baseline

May 3, 2011

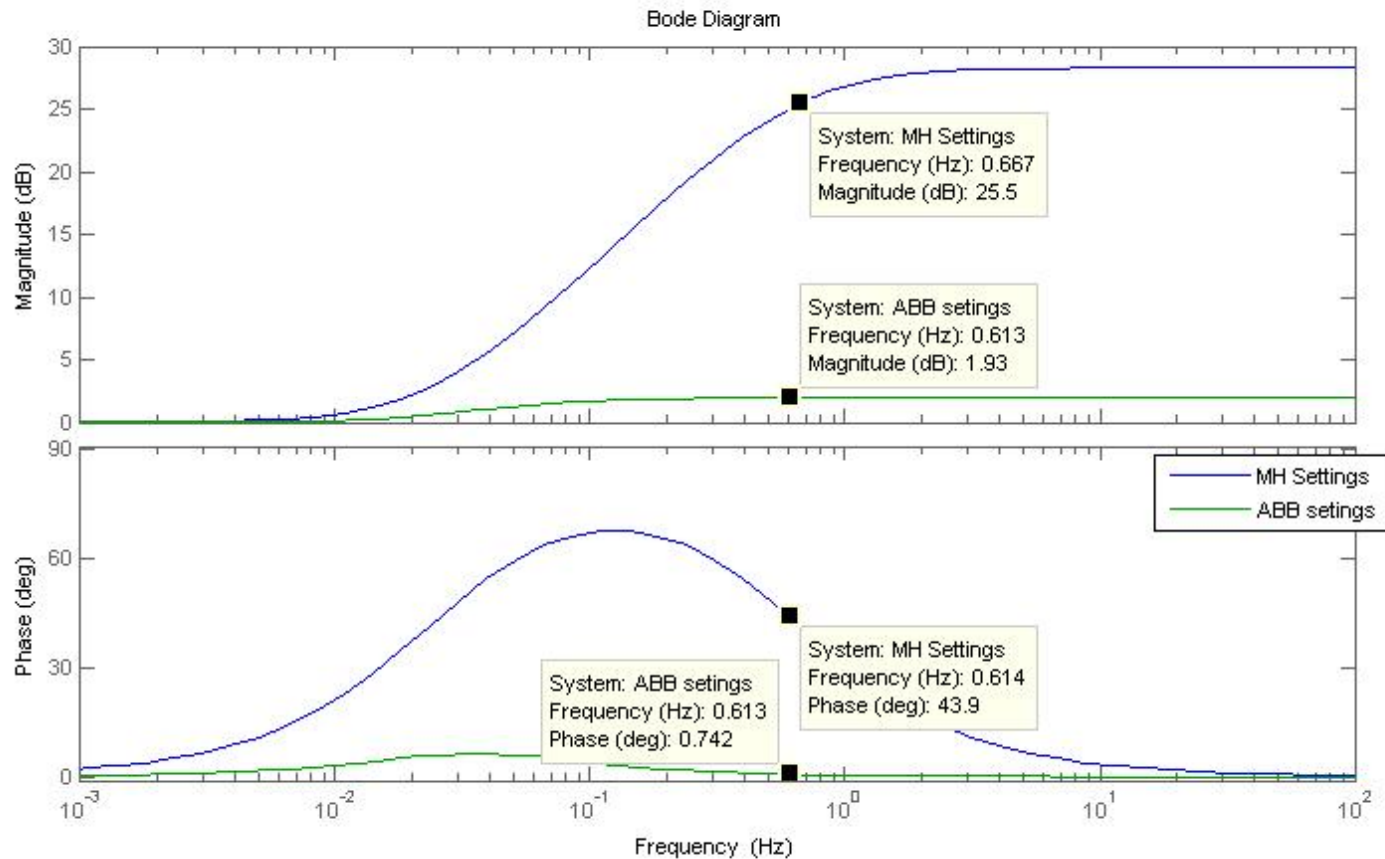


# Cont....System Baseline

May 25, 2011

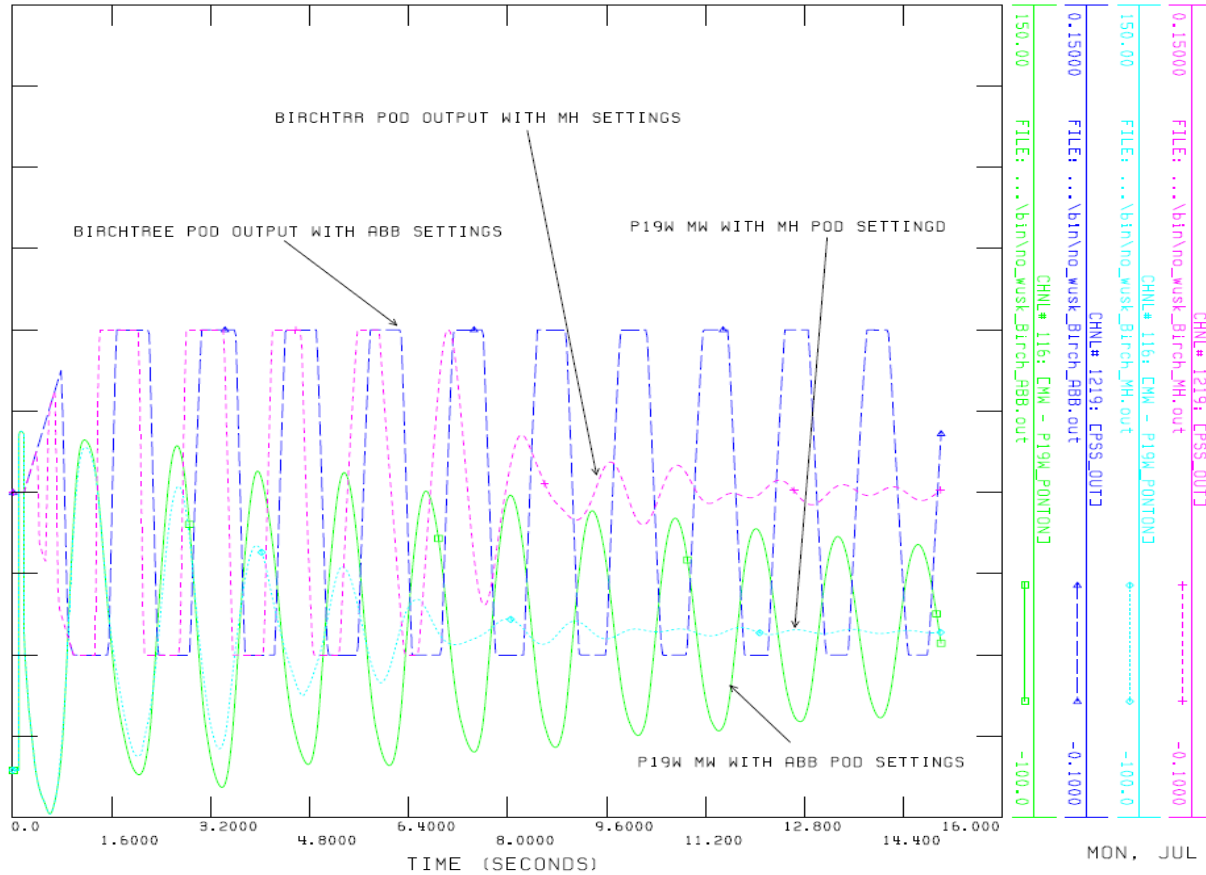


# Bode Plot (Lead /lag Block)



# Simulation Results

## Time Domain



KT2KS7JP6MK3.PM270.109:KT/KL/JP>2/7/6; INC 0 AVGE> PF AVG  
KETHC 204 ; KLSY 314; JNPG 168; MUSK 213; PSP 286; P19W 270 S0

MON, JUL 18 2011 12:21  
NO WUSK

Birchtree SVC System A  
Power Oscillation Damper

**General**

On / Off: **ON**

POD Input 1 - Delta Frequency: **ON**

POD Input 2 - Not used: **Not used**

Frequency Upper Limit: **61.0** Hz

Frequency Lower Limit: **59.6** Hz

**Washout**

Wash Out Filter 1:  $T_{w1}$  **10.000**

Wash Out Filter 2:  $T_{w2}$  **10.000**

**Lead / Lag**

Lead-lag Filter 1:  $T_{p1}$  **6.49000**

Lead-lag Filter 1:  $T_{z1}$  **0.25000**

Lead-lag Filter 2:  $T_{p2}$  **0.00000**

Lead-lag Filter 2:  $T_{z2}$  **0.00000**

Lead-lag Filter 3:  $T_{p3}$  **0.00000**

Lead-lag Filter 3:  $T_{z3}$  **0.00000**

**FILTER**

Time Constant:  $T_{f1}$  **0.2500**

Time Constant:  $T_{f2}$  **5.0000**

**Limitation**

SDC Max Limit:  $V_{SDCmax}$  **0.015** pu

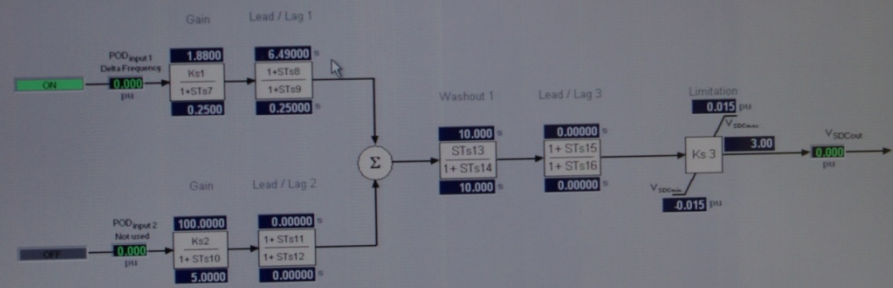
SDC Min Limit:  $V_{SDCmin}$  **0.015** pu

**Gain**

Input1 Gain:  $K_{s1}$  **1.8800**

Input2 Gain:  $K_{s2}$  **100.0000**

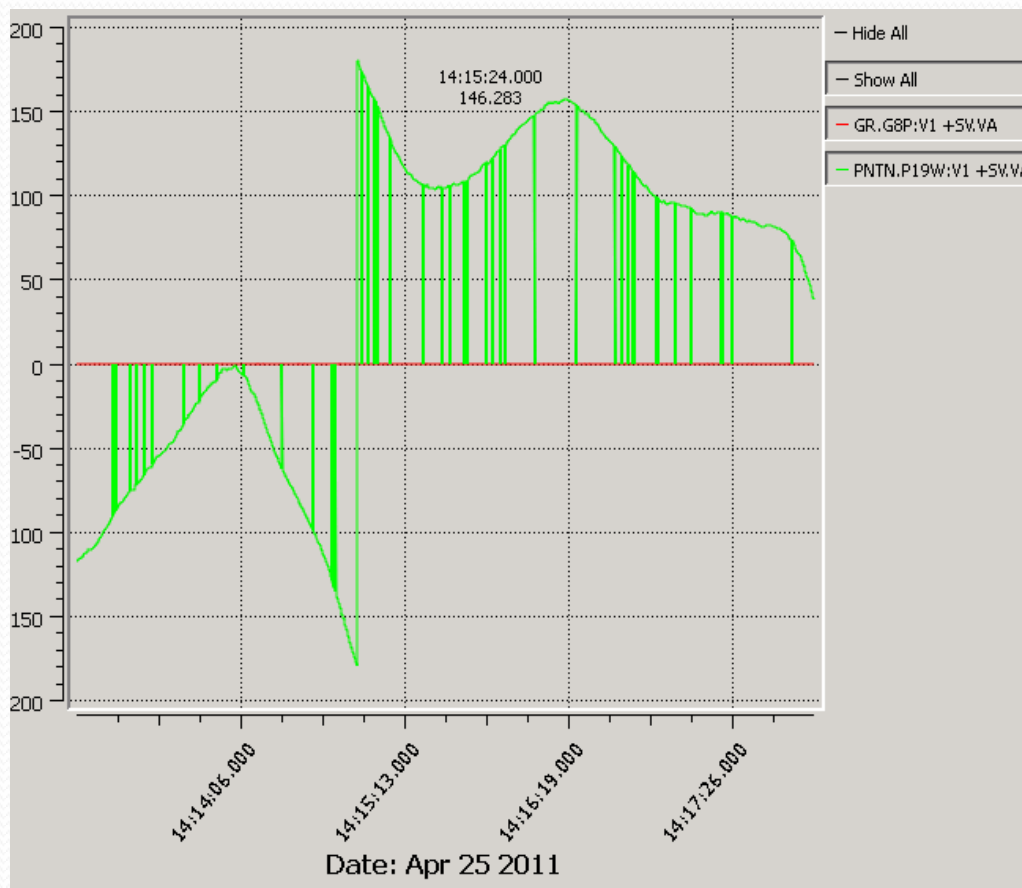
POD Gain:  $K_{s3}$  **3.00**





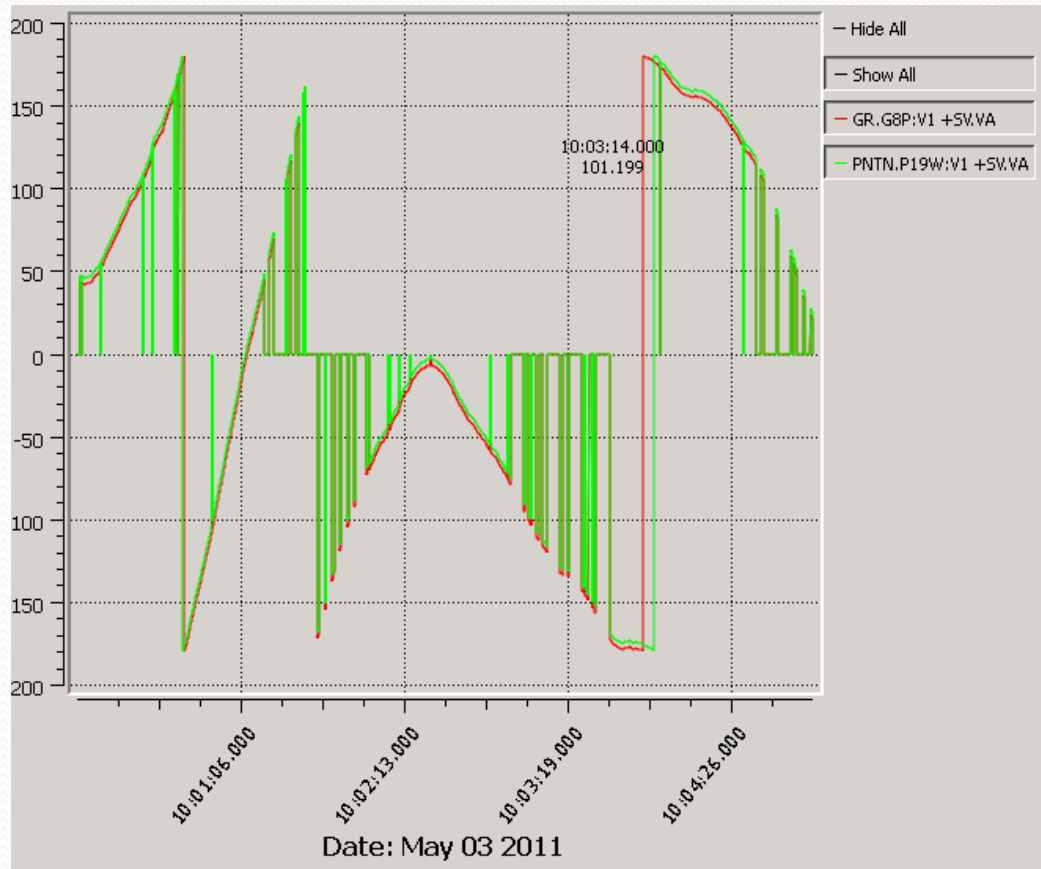
# Cont....System Baseline

April 25, 2011 – 13:13:00 to 13:18:00 – During the time of the Event

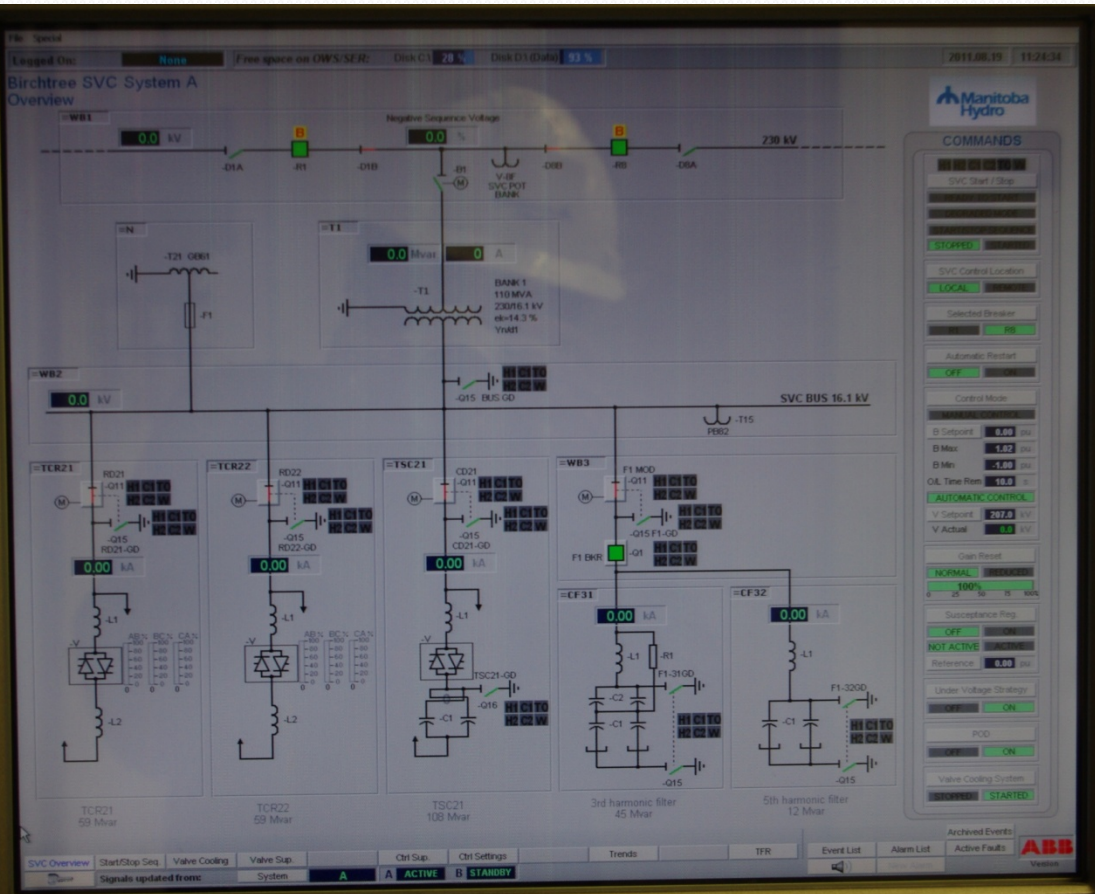


# Cont.....System Baseline

May 3, 2011 – 09:00:00 to 09:05:00 – About a week after the event







# Cont...Simulation Results

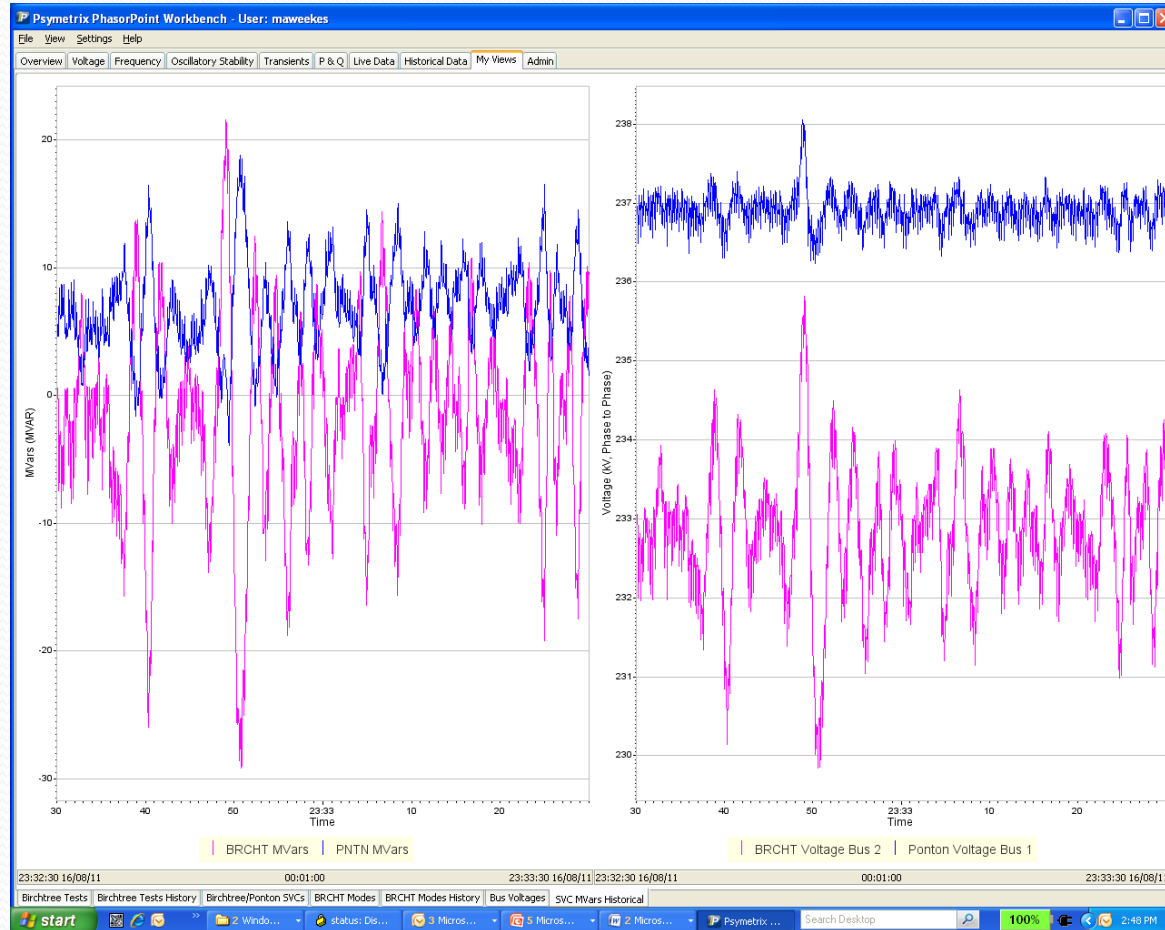
- Frequency Domain

MODAL COMPONENTS						
COMP. NO	EIGENVALUE		EIGENVECTOR		REMARKS	
	REAL	IMAGINARY	MAGNITUDE	ANGLE		
1	0.810635E-04	--	-104.72	--		
2	-0.149205	4.66803	16.997	-43.39	FREQ.:	0.743 HZ.
3	-9.23642	25.3357	2.1226	-85.51	FREQ.:	4.032 HZ.
4	-8.97202	42.6287	2.0465	-47.19	FREQ.:	6.785 HZ.
5	-0.212545	6.82925	1.4056	98.87	FREQ.:	1.087 HZ.
6	-7.89161	57.9493	0.98096	71.41	FREQ.:	9.223 HZ.
7	-5.64456	39.4219	0.66522	138.48	FREQ.:	6.274 HZ.
8	-0.895488	10.2439	0.47889	-124.57	FREQ.:	1.630 HZ.
9	-4.86058	61.9287	0.20336	-138.38	FREQ.:	9.856 HZ.
10	-1.22760	17.8970	0.17606	-20.57	FREQ.:	2.848 HZ.
11	-3.04154	50.4016	0.13071	9.49	FREQ.:	8.022 HZ.

# Commissioning tests

- Frequency sweep and discrete frequency injection
- MW transfer change
- 5% Step response of genertor exciter
- Open/ close line switching
- SLG Fault

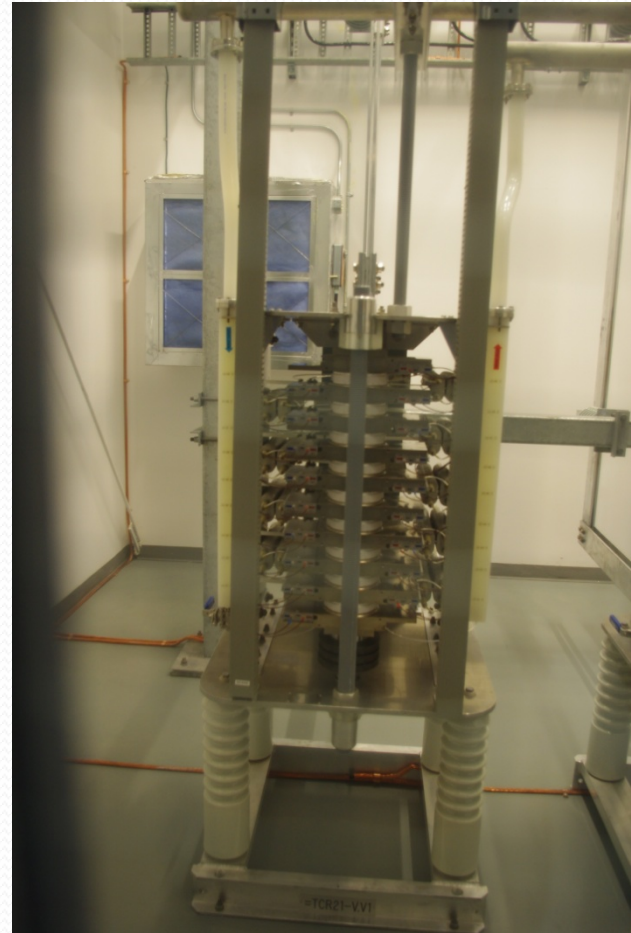
# Kettle Exciter Step Change



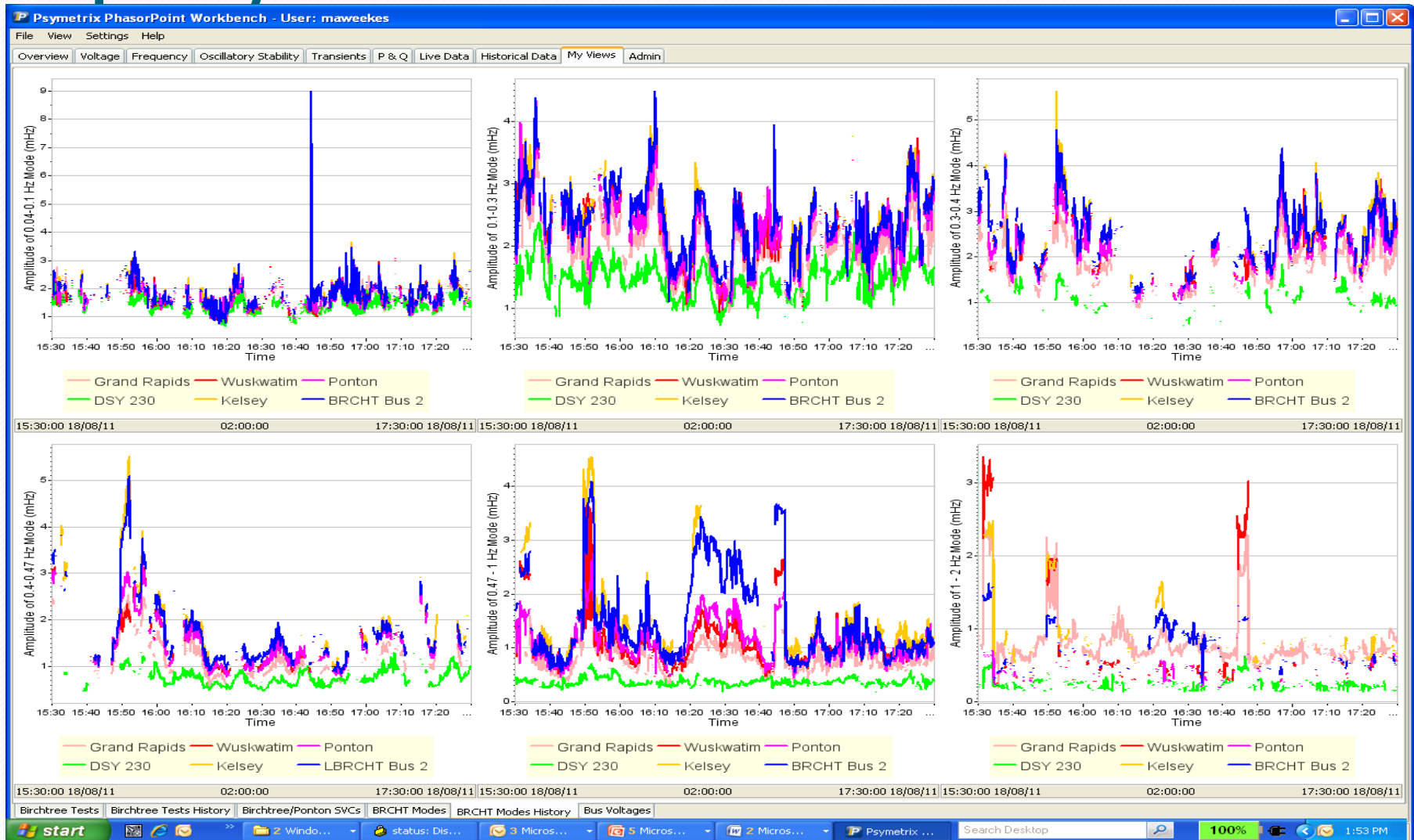
# Small-signal stability problems

- **Local plant mode oscillations:** Rotor angle oscillations of single generator or single plant against the rest of the system (0.7 to 2.0 Hz).
- **Intermachine/Interplant mode of oscillations:** Rotor angle oscillations between a few generator close to each other (0.7 to 2.0 Hz).
- **Interarea mode oscillations:** Oscillations of groups of generators in one area swinging against a groups of generators in another area (0.1 to 0.7 Hz).
- **Control mode oscillations:** Associated with control of equipment such as generator excitation systems (2.0 to 5.0 Hz).

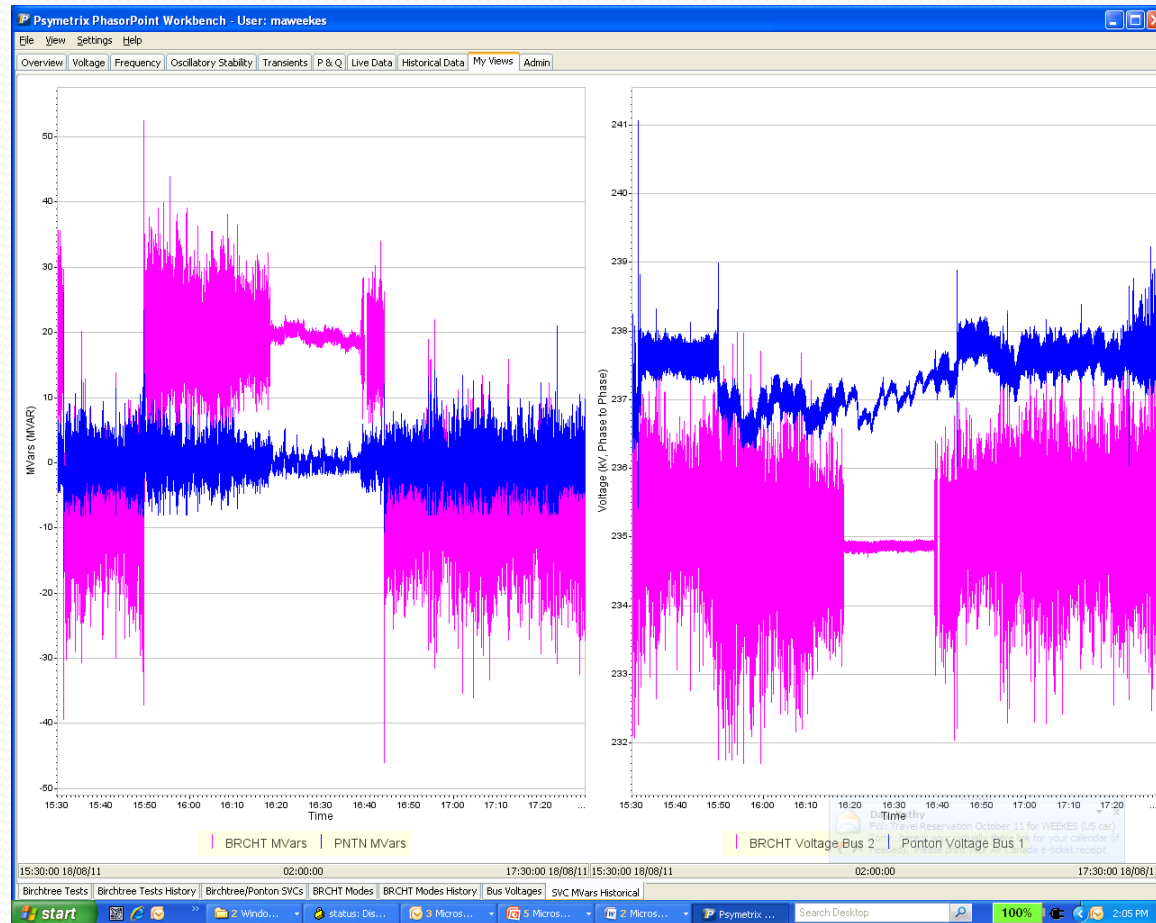




# Open/Close Line Test



# Open/Close Line test



# Commissioning Plan

- Time domain and frequency domain simulation studies
- System Baselineing (using the PMU and Psymetrix tools)
- Test schedule & planning
- Commissioning test process
- Results analysis